Computational Reconfigurable Imaging Spectrometer (CRISP)

Adam Milstein, Yaron Rachlin, Corrie Smeaton,
Ryan Sullenberger, Charles Wynn, Phil Chapnik, Steven Leman
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Overview of CRISP: Motivation Current IR Instruments for Earth Science

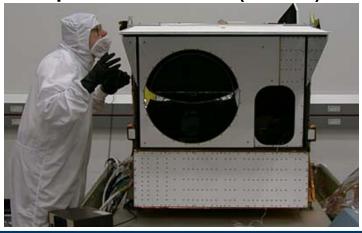
Atmospheric Infrared Sounder (NASA)



Weight 166 kg

Power 256 W

Moderate Resolution Imaging Spectroradiometer (MODIS)



Weight 228 kg

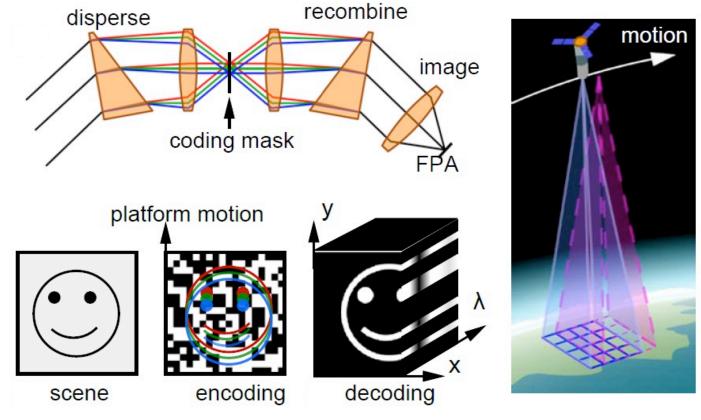
Power 162.5 W

- Spaceborne imagers and sounders have revolutionized understanding of weather and climate
- However, there are limitations in current design approaches
 - Expensive (\$>100's of millions)
 - Large (>100 kg)
 - Consume >100 watts
 - Long development cycle
 - · Failures catastrophic, cause long gap
 - Fewer instruments on-orbit limits revisit rate

Significant opportunity for new technology that can reduce size weight and power (SWaP)



Overview of CRISP: Our Approach



- Uses static mask and scan/platform motion to encode spectral data cube
- SWaP and SNR advantages over traditional designs



SNR of CRISP vs. SNR of Conventional Slit-Based Spectrometers

SNR comparison of CRISP to conventional pushbroom spectrometer

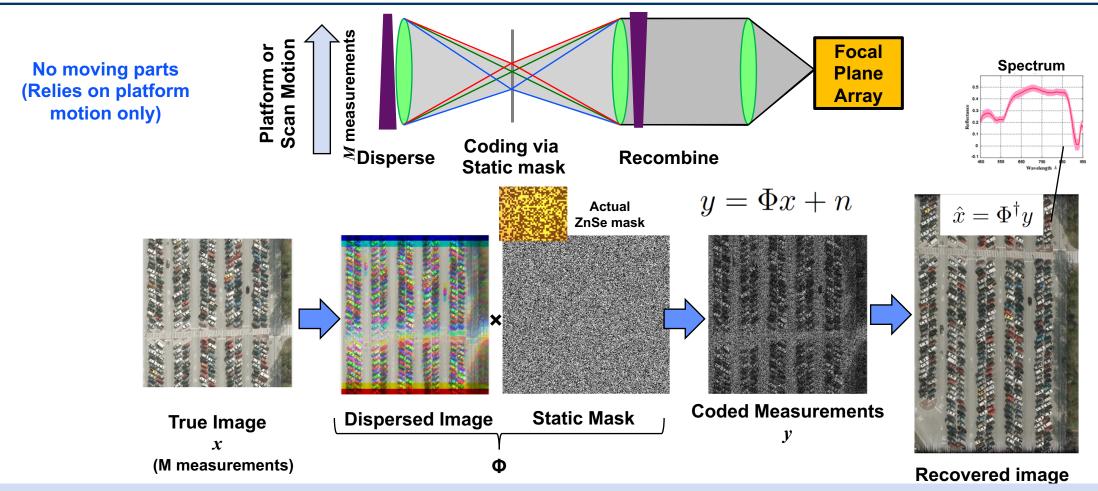
	Slit-based system SNR scaling	CRISP SNR scaling	Rationale	Note
Shot-noise limited (e.g., visible CCD, cooled MCT)	1	$\sim \sqrt{M/2N_{\lambda}}$ Example*: $\sim 6 \times$	Overdetermined measurement: $M > N_{\lambda}$ Traditional design: $N_{\lambda} = M$	Number of measurements: M Number of measured wavelengths: N_{λ}
Detector-noise limited (e.g., uncooled microbolometer)	1	$\sim \sqrt{M}/2$ Example*: $\sim 22 \times$	All λ measured at once; "multiplexing" advantage	

^{*}Example: $M = 1920, N_{\lambda} = 30$

CRISP enables significant SNR improvement over conventional designs



CRISP Spectral Decoding



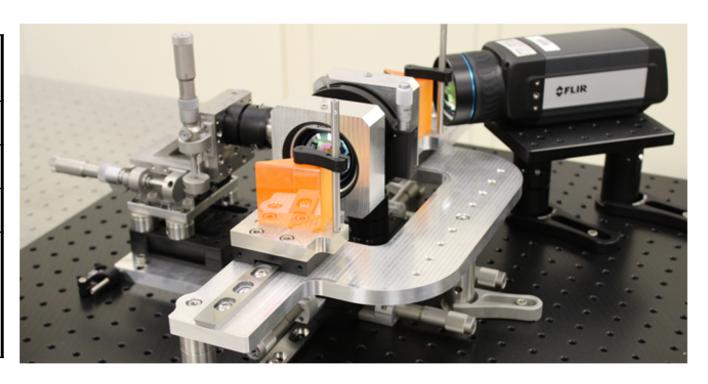
- CRISP more sensitive than dispersive + FTIR, for both shot-noise and detector-noise limited measurements
- CRISP advantage maximized with noisy detectors



Breadboard Measurements

λ	7.7 μm – 14 μm (67 pixel dispersion extent)
Δλ	0.14 um resolvable
D	5 cm
FOV	~15°

COTS f/1 camera lenses from FLIR Custom ZnSe prisms Custom designed mounts and baffles

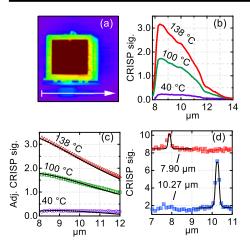


Use COTS based system to validate model predictions

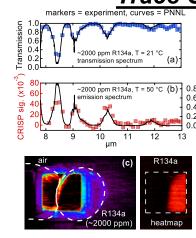


Breadboard: Example Measured Spectra

Extended and Narrowband Source Example



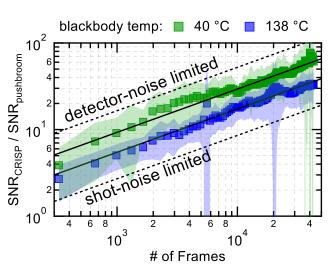
Trace Gas Example



 Breadboard measurements to date have shown good qualitative spectral reconstructions of narrowband, blackbody, and gas targets



Breadboard Measurements: SNR Scaling

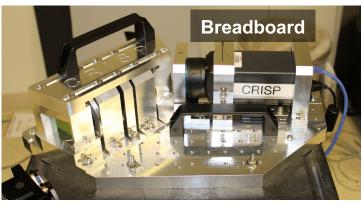


- SNR scaling with \sqrt{M} is confirmed, with improvement relative to comparable slit based system
- Factor of ~2 lower than theoretical limit for binary mask when detector noise limited
 - Departure from binary system function appears to account for this
 - Additional SNR scaling measurements planned for all configurations



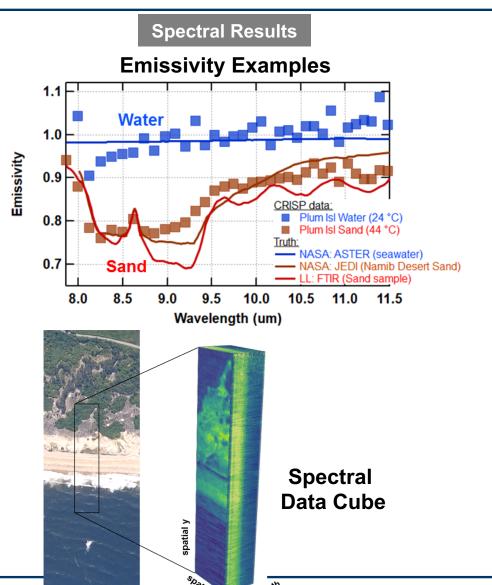
Breadboard Measurements: (Internally Funded) Flight Data and Functional Demo







CRISP works on real moving platform, and distinguishes spectra of different materials in high-contrast scene



LINCOLN LABORATORY

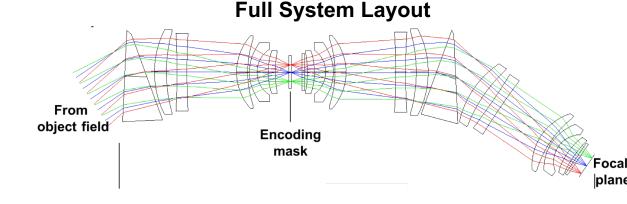
MASSACHUSETTS INSTITUTE OF TECHNOLOGY



Brassboard Design

- Brassboard designed for in-depth field testing
 - Custom optics, with high image quality over entire FOV
 - As-built lenses are predicted to be diffraction limited with commercial-grade fabrication tolerances
 - Telecentric design provides uniform image illumination
 - Design informed by breadboard and model insights
- Design close to complete
 - Optical design 90% completed
 - Optomechanics design 80% completed
 - Future modifications will accommodate reconfigurability

Brassboard is close to a complete design, and is well-positioned for future development

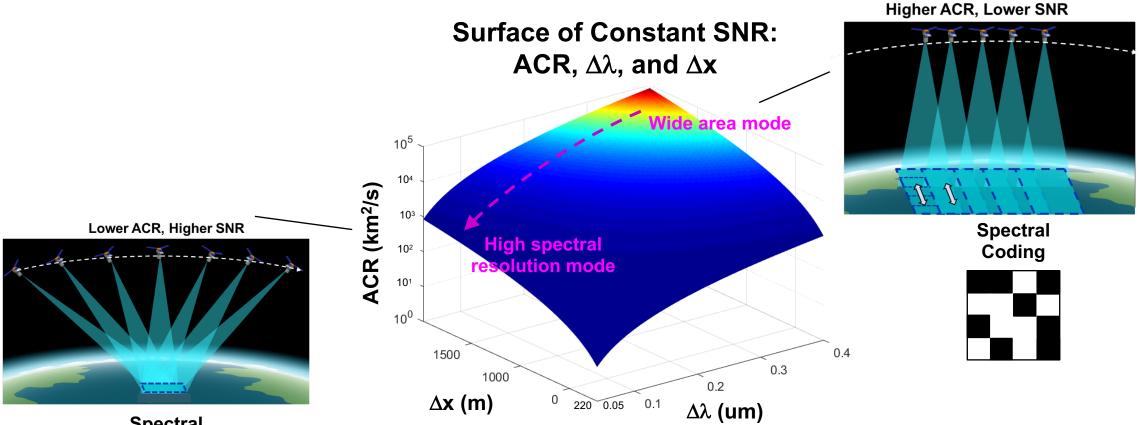


Lens Barrel





Spatial and Spectral Reconfigurability



Spectral Coding



- With change of mask and CONOPS, CRISP can be reconfigured to respond to new observations by applying different spatial/spectral encoding design
- Trade off area coverage rate, spatial resolution and spectral resolution



Summary of Technical Efforts and Findings to Date

- Developed model of proposed CRISP system, and used model to predict performance
 - SNR scaling, impact of aberrations, spectral/spatial resolution, encoding/decoding process
- Validated these models with laboratory demonstration on breadboard
 - Validated model will guide formulation of future system designs
- Completed 80-90% of design work for proposed brassboard
- Current emphasis on reconfigurability and model validation
 - Allow variation of spatial and spectral capabilities on-orbit
 - Validate models with laboratory demonstrations (indoor and out)
 - Identify performance limits

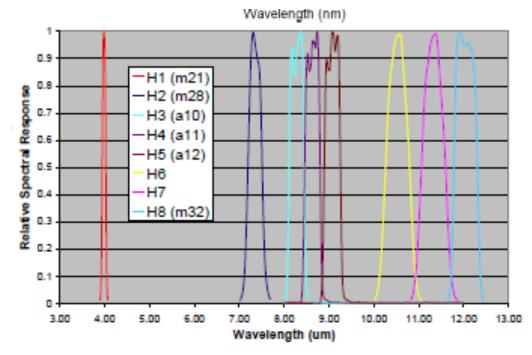


Toward Science Applications

Thermal Imager Bands and Science Applications [1]

	,
λ Range (μm)	Products
7.22-7.44	Lower-level water vapor, winds, SO2
8.3-8.7	Total water for stability, cloud phase, dust, SO2, rainfall
9.42-9.8	Total ozone, turbulence, and winds
10.1-10.6	Surface and cloud
10.8-11.6	Imagery, SST, clouds, rainfall
11.8-12.8	Total water, ash, and SST
13.0-13.6	Air temperature, cloud heights and amounts

Surface Biology and Geology HySPIRI TIR Bands [2]



Surface temperature and emissivity for volcanoes, wildfires, water use and availability, urbanization, land surface composition and change

· CRISP potentially addresses several science needs in thermal IR band

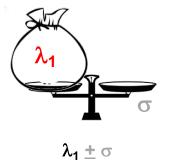


Backup



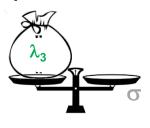
Multiplexing Advantage Illustration

Pushbroom Spectrometer





 $\lambda_2 \pm \sigma$



 $\lambda_3 \pm \sigma$

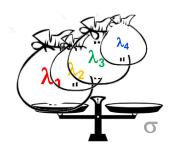


 $\lambda_4 \pm \sigma$

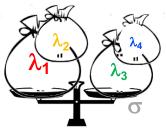
Measure each λ independently

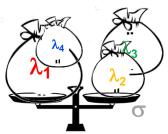
Error at each $\lambda =$ detector noise (σ)

Multiplex Spectrometer









Measure linear combinations of λ s

$$(\lambda_4 + \lambda_2 + \lambda_3 + \lambda_4) + \sigma$$

$$(\lambda_1 + \lambda_2 + \lambda_3 + \lambda_4) \pm \sigma \qquad (\lambda_1 - \lambda_2 + \lambda_3 - \lambda_4) \pm \sigma$$

$$(\lambda_1 + \lambda_2 - \lambda_3 - \lambda_4) \pm \sigma$$

$$(\lambda_1 - \lambda_2 - \lambda_3 + \lambda_4) \pm \sigma$$

"Encoding"

"Inversion"

$$\begin{array}{l} \lambda_1 = \frac{1}{4} \left(\mathbf{M}_1 + \mathbf{M}_2 + \mathbf{M}_3 + \mathbf{M}_4 \right) \\ \lambda_2 = \frac{1}{4} \left(\mathbf{M}_1 - \mathbf{M}_2 + \mathbf{M}_3 - \mathbf{M}_4 \right) \\ \lambda_3 = \frac{1}{4} \left(\mathbf{M}_1 + \mathbf{M}_2 - \mathbf{M}_3 - \mathbf{M}_4 \right) \\ \lambda_4 = \frac{1}{4} \left(\mathbf{M}_1 - \mathbf{M}_2 - \mathbf{M}_3 + \mathbf{M}_4 \right) \end{array}$$

$$\sigma_{\lambda 1}^2 = \frac{1}{4}(\sigma^2 + \sigma^2 + \sigma^2 + \sigma^2) \qquad \sigma_{\lambda 1} = \frac{1}{2}\sigma$$

$$\sigma_{\lambda 2}^2 = \frac{1}{4}(\sigma^2 + \sigma^2 + \sigma^2 + \sigma^2) \qquad \sigma_{\lambda 2} = \frac{1}{2}\sigma$$

Measurement errors*

Error at each λ = $\frac{1}{\sqrt{2}}$ *detector noise (σ) # of detectors

^{*} Errors add in quadrature: If x = x1 + x2 + ... then $\sigma_{x^2} = \sigma_{x1^2} + \sigma_{x2^2} + ...$ Multiplicative constant multiplies error: If x = Ax1, then $\sigma_x = A\sigma_{x1}$